

SIEMENS

ARRAYCON

GUI Tool & FEM modeling

ZhongZhe DONG

GUI tool

Summary

- Calculate the eigen functions/values
 - Isotropic/orthotropic plate
 - Multiple boundary conditions
- Illustrate physical modes
 - Single modes
 - Modes super-position
- Simulate the excitation response
 - Without damping
 - Chose excitation location
 - Chose exciting time and measure time

GUI tool

Interface

Plate size

Vibration set

Material

Boundary condition

Excitation set

Eigenfrequencies & modes

Interface

Panel size

Length [m] Width [m]

Thickness [m] Enter

Material properties

Ex [Pa] Ey [Pa]

Gxy [Pa] Poisson

Density [Kg/m-3] Enter

Excitation set

0.1 0.222

0 100

Enter

Vibration set

Ramps in x direction Ramps in y direction

Enter

Boundary conditions

clamped-clamped

clamped-clamped

Modes

30.48084
55.81733
96.63738
69.83944
92.75549
131.5403
129.7192
151.6955
188.9682

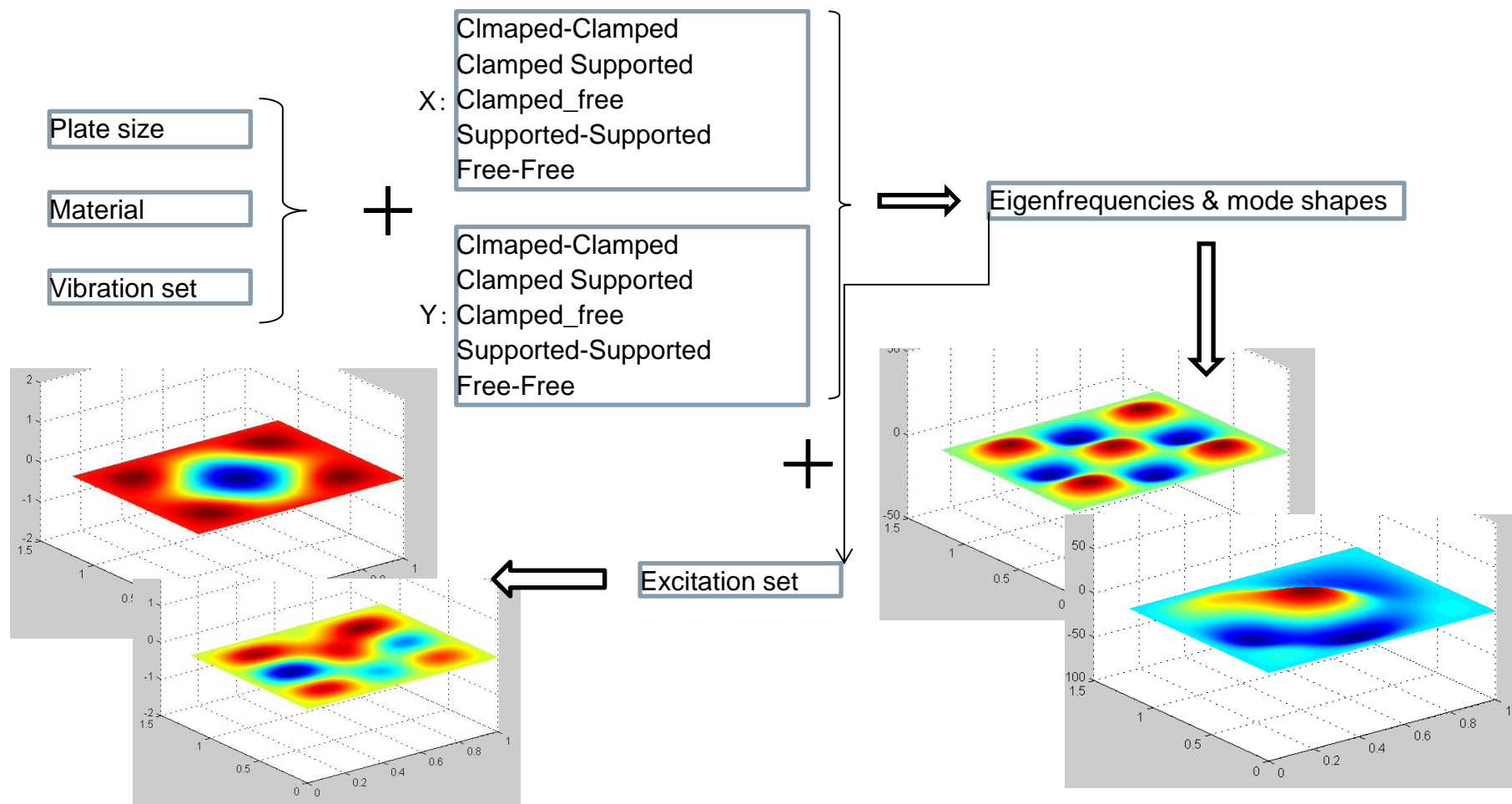
Enter

Analysis

Analyse

How does it work?!

Interface



Green function

Deflection of the plate

$$W_{(x,y,t)} = \sum_{m=1}^{\infty} \sum_{n=1}^{\infty} \phi_m(x) \psi_n(y) C_{mn} e^{j\Omega_{mn}t}$$

Velocity:

$$\dot{W}_{(\bar{x},\bar{y},t)} = \sum_{m=1}^{\infty} \sum_{n=1}^{\infty} j\Omega_{mn} \phi_m(\bar{x}) \psi_n(\bar{y}) C_{mn} e^{j\Omega_{mn}t}$$

Initial condition:

$$\begin{aligned} \dot{W}_{(\bar{x},\bar{y},0)} &= \sum_{m=1}^{\infty} \sum_{n=1}^{\infty} j\Omega_{mn} \phi_m(x) \psi_n(y) C_{mn} \\ \Rightarrow C_{mn} &= \frac{1}{j\Omega_{mn}} \iint \dot{W}_{(\bar{x},\bar{y},t=0)} \phi_m(\bar{x}) \psi_n(\bar{y}) d\bar{x} d\bar{y} \end{aligned}$$

Green function

Deflection of the plate:

$$W_{(x,y,t)} = \sum_{m=1}^{\infty} \sum_{n=1}^{\infty} \phi_m(x) \psi_n(y) C_{mn} e^{j\Omega_{mn}t}$$

Deflection of the plate with initial condition:

$$W_{(x,y,t)} = \sum_{m=1}^{\infty} \sum_{n=1}^{\infty} \phi_m(x) \psi_n(y) e^{j\Omega_{mn}(t)} \frac{1}{j\Omega_{mn}} \iint W_{(\bar{x},\bar{y},0)} \phi_m(\bar{x}) \psi_n(\bar{y}) d\bar{x} d\bar{y}$$

Deflection of the plate with initial condition:

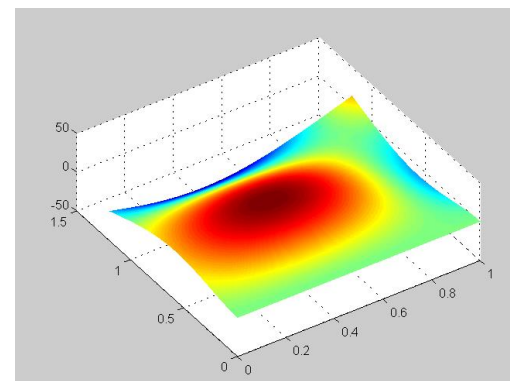
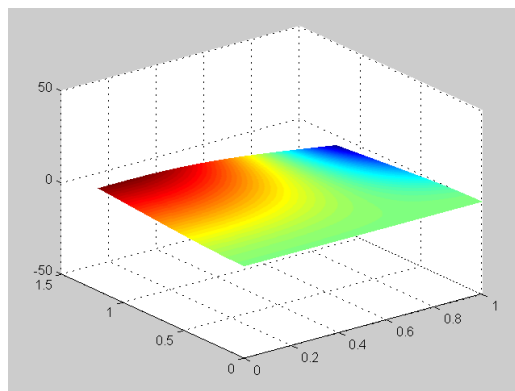
$$W_{(x,y,t)} = \int \sum_{m=1}^{\infty} \sum_{n=1}^{\infty} \phi_m(x) \psi_n(y) e^{j\Omega_{mn}(t-\tau)} \frac{1}{j\Omega_{mn}} \iint f \phi_m(\bar{x}) \psi_n(\bar{y}) d\bar{x} d\bar{y} d\tau$$

Different boundary conditions mode shape

CFFF & CFCF

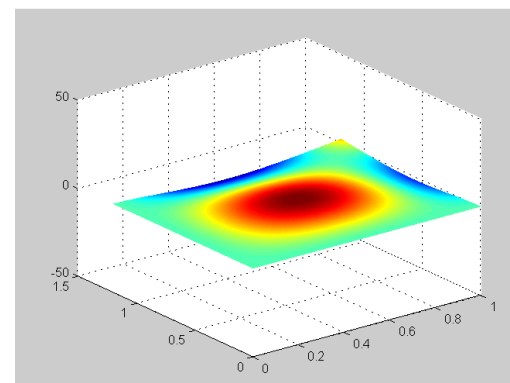
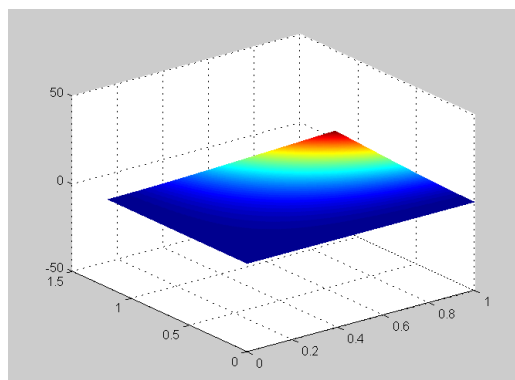
74.3Hz

273.9Hz



35.3Hz

208.8Hz

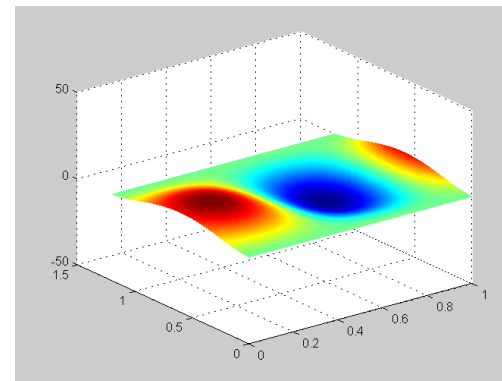
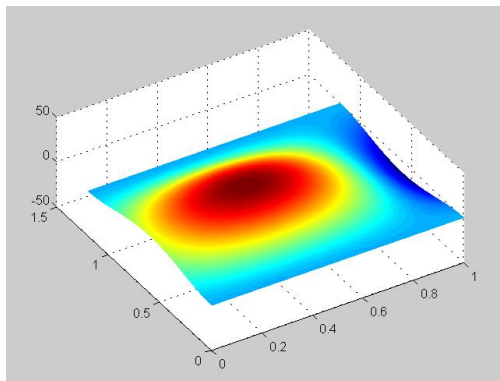


Different boundary conditions mode shape

CCFF & CCSS

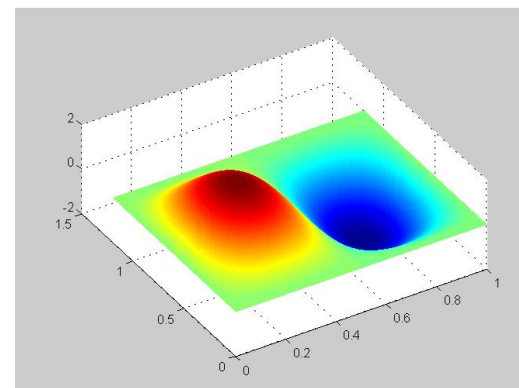
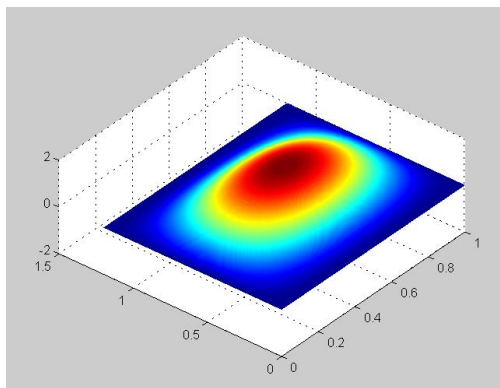
275.2Hz

449.7Hz



235.48Hz

470.8Hz

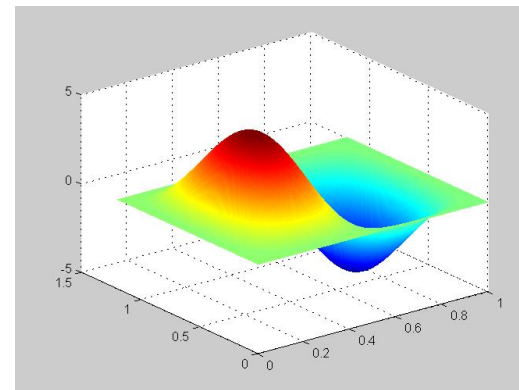
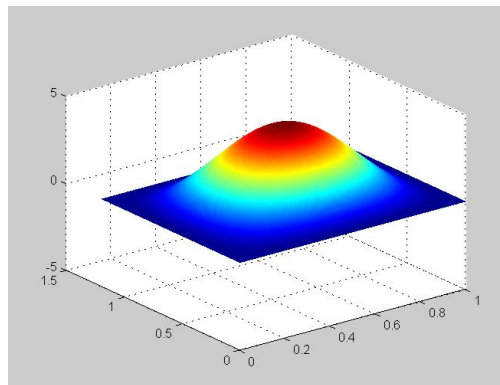


Different boundary conditions mode shape

CCCC & SSSS

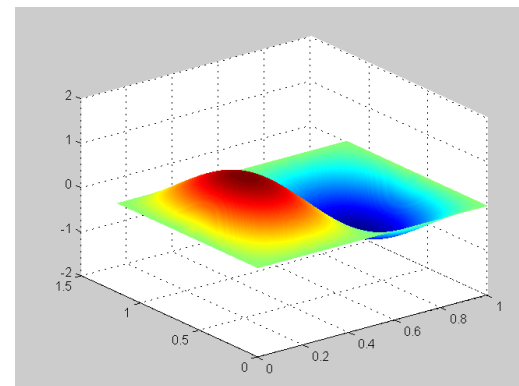
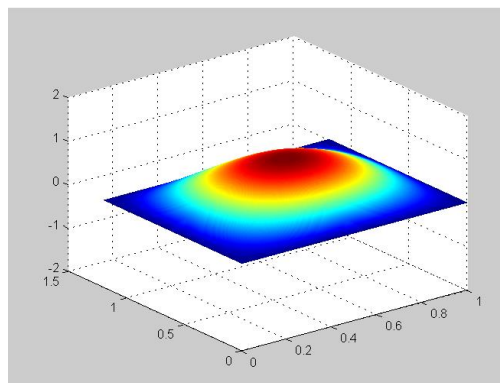
309.5Hz

566.8Hz



172.1Hz

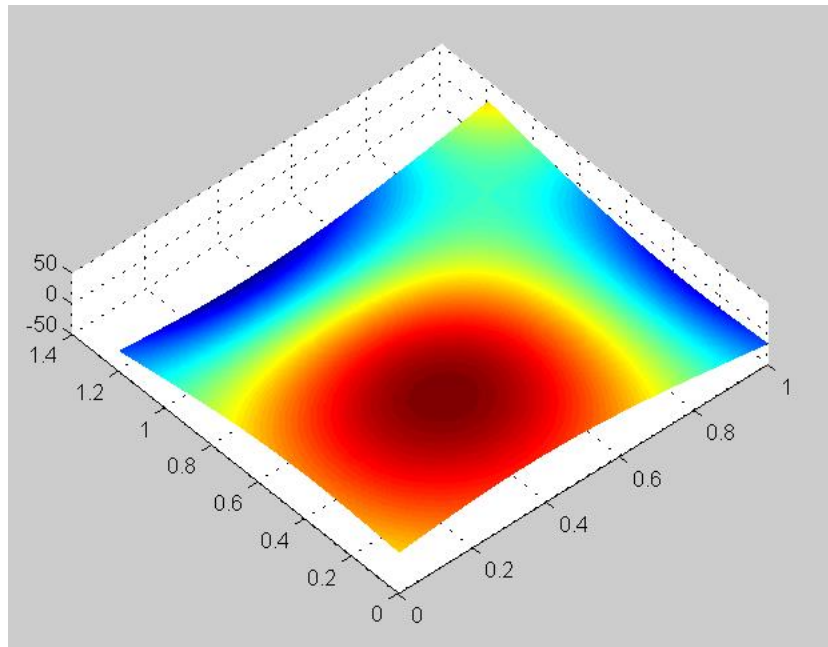
383.8Hz



FFFF mode shape...

Boundary condition: free-free

- Not a symmetric form
 - No spacial restraint
 - Depend on the initial value of the Newton iteration method in the code



Piezoelectric effect coupling

For the plate:

Neutral surface location

$$\int_{-\frac{t_s}{2}}^{\frac{t_s}{2}} \frac{E_s(z-\delta)}{r} dz + \int_{\frac{t_s}{2}}^{\frac{t_s}{2}+t_p} \frac{E_p(z-\delta)}{r} dz = 0$$

- In plane forces

$$N_x = -K_t \left(\frac{\partial^2 w}{\partial x^2} + \nu_t \frac{\partial^2 w}{\partial y^2} \right) + \int_{\frac{t_s}{2}}^{\frac{t_s}{2}+t_p} e_3 d_{31} dz = 0$$

$$N_y = -K_t \left(\frac{\partial^2 w}{\partial y^2} + \nu_t \frac{\partial^2 w}{\partial x^2} \right) + \int_{\frac{t_s}{2}}^{\frac{t_s}{2}+t_p} e_3 d_{32} dz = 0$$

So

$$K_t \left(\frac{\partial^2 w}{\partial x^2} + \nu_t \frac{\partial^2 w}{\partial y^2} \right) = e_3 t_p d_{31}$$

$$K_t \left(\frac{\partial^2 w}{\partial y^2} + \nu_t \frac{\partial^2 w}{\partial x^2} \right) = e_3 t_p d_{32}$$

Plate FEM modeling

Mass, stiffness, voltage matrix

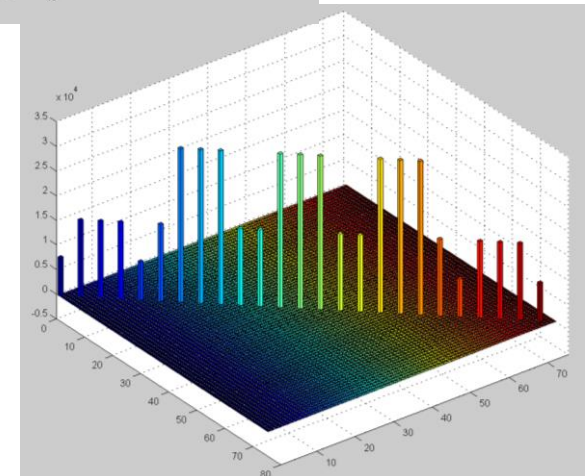
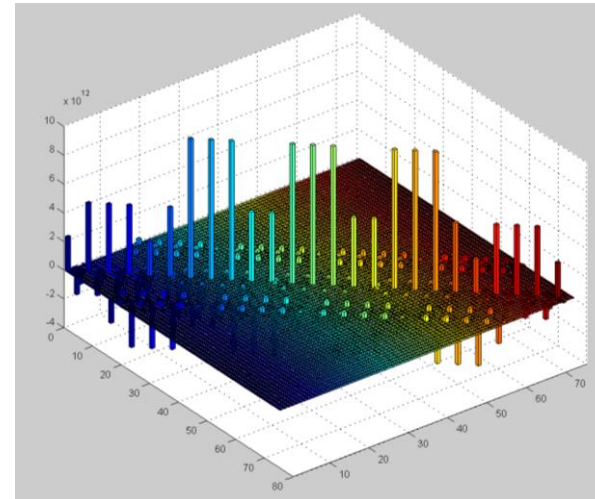
$$\mathbf{m} = \int_{V_s} \mathbf{B}_\eta^t \mathbf{Z}^t \rho_s \mathbf{Z} \mathbf{B}_\eta dV_s + \int_{V_p} \mathbf{B}_\eta^t \mathbf{Z}^t \rho_p \mathbf{Z} \mathbf{B}_\eta dV_p$$

$$\mathbf{k} = \int_{V_s} z^2 \mathbf{B}_\kappa^t \bar{\mathbf{c}}_s \mathbf{B}_\kappa dV_s + \int_{V_p} z^2 \mathbf{B}_\kappa^t \bar{\mathbf{c}}_p^E \mathbf{B}_\kappa dV_p$$

$$\boldsymbol{\theta} = \int_{V_p} z \mathbf{B}_\kappa^t \bar{\mathbf{e}}^t \mathbf{B}_E dV_p$$

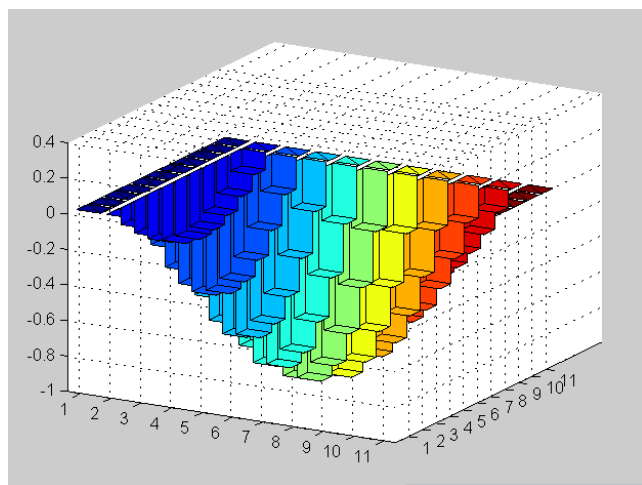
$$\mathbf{M} \ddot{\boldsymbol{\Psi}} + \mathbf{C} \dot{\boldsymbol{\Psi}} + \mathbf{K} \boldsymbol{\Psi} - \boldsymbol{\Theta} \mathbf{v} = \mathbf{F}$$

$$\mathbf{C}_p \mathbf{v} + \mathbf{Q} + \boldsymbol{\Theta}^t \boldsymbol{\Psi} = 0$$

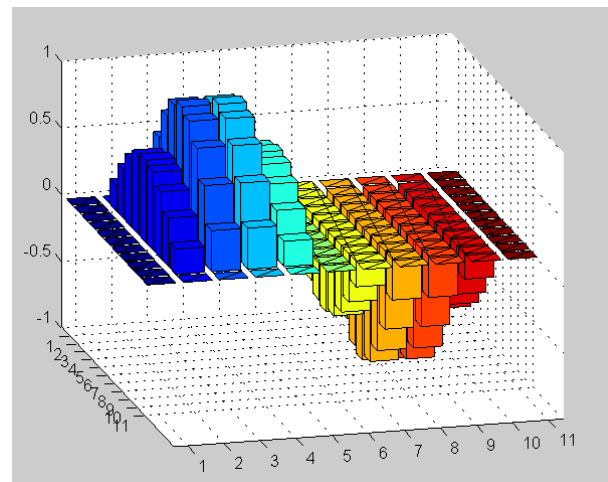


First results

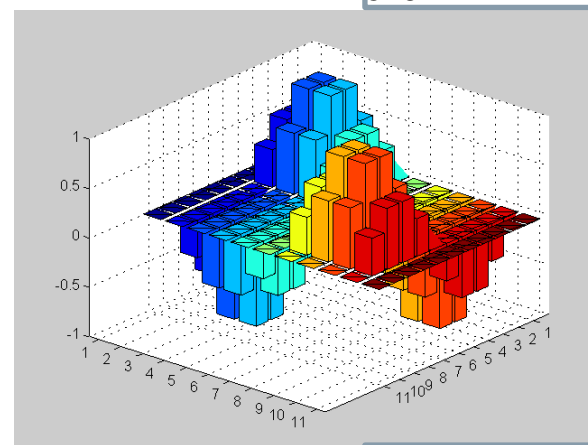
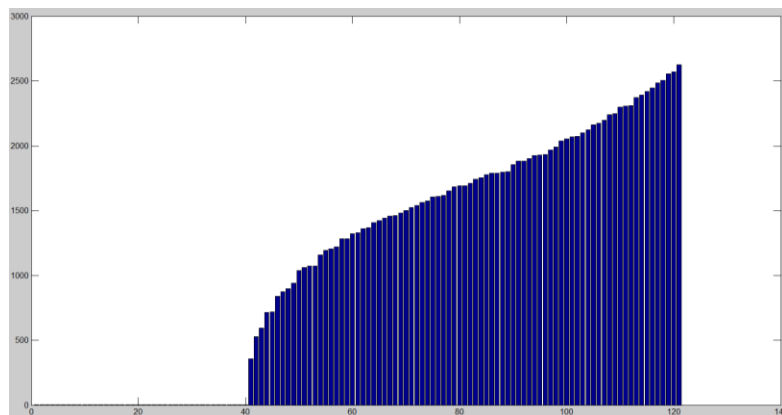
First two mode shapes by FEM without electromechanical coupling



357.9Hz



526.7Hz



716.2Hz

Improving

Summary

- GUI tool
 - Calculation Method (Newton)
 - Structure of the GUI
- FEM modeling
 - Continuing to work
 - Piezoelectric effect coupling
- Paper
 - Result of the mechanical effect by adding extra patches
 - FEM modeling result